

**IN THE SPECIFICATION**

**Please replace the paragraph beginning at page 10, line 23, with the following amended paragraph:**

When a flow rate  $A(\text{sccm})$  [sccm is a volumetric flow rate ( $\text{cm}^3/\text{min}$ ) at a reference temperature the standard condition of the ideal gas, and  $A(\text{sccm})$  is equal to  $A \times 10^{-6}$  ( $\text{m}^3/\text{min}$ )] of the CF based gas running through the processing chamber 2 is, i.e.,  $7.44 \times 10^{-7} A(\text{mol/sec})$ , a CF based gas corresponding to 20% of the CF based gas flow rate, i.e.,  $7.44 \times 10^{-7} A \times 0.2 = 1.49 \times 10^{-7} A(\text{mol/sec})$ , is left in the processing chamber 2, based on a relation between the exhausting capacity of the vacuum pump 56 and a mass flow corresponding to F included in CF based gas running through the processing chamber 2.

**Please replace the paragraph beginning at page 11, line 7, with the following amended paragraph:**

Further, given that the ratio of 'a' to the degree of polymerization (X) of the  $\text{CF}_2$  polymer is 2 in reaction equations 1 to 3 and the ratio of 'f' to the degree of polymerization (X) of the  $\text{CF}_2$  polymer is 3 in reaction equation 4 even if all of CF based gas is converted into the  $\text{CF}_2$  polymer, the moles of  $\text{Y}_2\text{O}_3$  sprayed coating 41 required per unit time are  $1.49 \times 10^{-7} A(\text{mol/sec}) \times 0.66 = 9.92 \times 10^{-8} A(\text{mol/sec})$  corresponding to 66% ( $2 \times 1/3$ ) of the moles corresponding to the flow rate of the CF based gas remaining in the processing chamber 2.

**Please delete the original Abstract on page 20, and replace it with the following Abstract:**